

Data Sheet July 23, 2003 FN7374

### **Dual Push-Pull Laser Driver Oscillator**

# élantec.

The EL6208 is a dual push-pull oscillator used to reduce laser noise in twin laser diodes. It uses the standard

interface to existing ROM controllers. The frequency and amplitude are both set with a separate resistor connected to ground. The tiny package and harmonic reduction allow the part to be placed close to a laser with low RF emissions. An auto turn-off feature allows activates the oscillator only when the APC current is applied.

If the APC current is reduced such that the average laser voltage drops to less than 1.1V, the output and oscillator are disabled, reducing power consumption to a minimum.

The current drawn by the oscillator consists of a small utility current, plus the peak output amplitude in the positive cycle. In the negative cycle the oscillator subtracts peak output amplitude from the laser APC current. The waveform is filtered to reduce EMI emissions.

The EL6208 operates from a signal +5V supply. Power consumption is very low. The EL6208 part is available in the space-saving 6-pin SOT-23 package and is specified for operation from 0°C to +70°C.

# **Ordering Information**

PART NUMBER	PACKAGE	TAPE & REEL	PKG. DWG. #
EL6208CW-T7	6-Pin SOT-23	7" (3K pcs)	MDP0038
EL6208CW-T7A	6-Pin SOT-23	7" (250 pcs)	MDP0038

#### **Features**

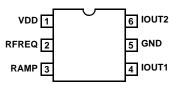
- · Low power dissipation
- User-selectable frequency from 60MHz to 600MHz controlled with a single resistor
- User-specified amplitude from 10mA<sub>PK-PK</sub> to 100mA<sub>PK-PK</sub> controlled with a single resistor
- · Auto turn-off threshold
- Soft edges for reduced EMI
- · Small 6-pin SOT-23 package

### **Applications**

• CD-DVD ROM drives

### **Pinout**

**EL6208** (6-PIN SOT-23) TOP VIEW



### **Absolute Maximum Ratings** (T<sub>A</sub> = 25°C)

### Voltages Applied to: V<sub>DD</sub> . . . . . -0.5V to +6.0V I<sub>OUT</sub> . . . . . -0.5V to +6.0V $R_{\mbox{\scriptsize FREQ}}, R_{\mbox{\scriptsize AMP}}$ .....-0.5V to +6.0V Operating Ambient Temperature Range ..... 0°C to +70°C Storage Temperature Range . . . . . . . . . . . . . -65°C to +150°C Power Dissipation (max) . . . . . . . . . . See Curves

### **Recommended Operating Conditions**

V <sub>DD</sub>	 	5V ±10%
V <sub>OUT</sub>	 	2V - 3V
R <sub>FREQ</sub>	 	$\dots$ 3K $\Omega$ (min)
R <sub>AMP</sub>	 	$1.25k\Omega$ (min)
F <sub>OSC</sub>	 	60-600MHz
$I_{\text{OUT}},\dots,$	 	10-100mA <sub>PK-PK</sub>

CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

IMPORTANT NOTE: All parameters having Min/Max specifications are guaranteed. Typical values are for information purposes only. Unless otherwise noted, all tests are at the specified temperature and are pulsed tests, therefore:  $T_J = T_C = T_A$ 

Supply & Reference Voltage Characteristics  $V_{DD} = +5V$ ,  $T_A = 25^{\circ}C$ ,  $R_L = 10\Omega$ ,  $R_{FREQ} = 5210\Omega$  ( $F_{OSC} = 360MHz$ ),  $R_{AMP} = 1000$  $2540\Omega$  (I<sub>OUT</sub> =  $50mA_{P-P}$  measured at 60MHz), V<sub>OUT</sub> = 2.2V

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
PSOR	Power Supply Operating Range		4.5		5.5	V
I <sub>SO</sub>	Supply Current Disabled	V <sub>OUT</sub> < V <sub>CUTOFF</sub>		280	440	μA
I <sub>STYP</sub>	Supply Current Typical Conditions	$R_{FREQ} = 5.21k\Omega$ , $R_{AMP} = 2.54k\Omega$		20	23	mA
I <sub>SLO</sub>	Supply Current Low Conditions	$R_{FREQ} = 18.2k\Omega$ , $R_{AMP} = 12.7k\Omega$		5.4		mA
I <sub>SHI</sub>	Supply Current High Conditions	$R_{FREQ} = 3.3k\Omega$ , $R_{AMP} = 1.27k\Omega$		36.8		mA
V <sub>FREQ</sub>	Voltage at R <sub>FREQ</sub> Pin			1.27		V
V <sub>RAMP</sub>	Voltage on R <sub>AMP</sub> Pin			1.27		V
V <sub>CUTOFF</sub>	Monitoring Voltage of I <sub>OUT</sub> Pin		1.1		1.4	V

# $\textbf{Oscillator Characteristics} \quad \text{$V_{DD} = +5V$, $T_{A} = 25^{\circ}C$, $R_{L} = 10\Omega$, $R_{FREQ} = 5210\Omega$ ($F_{OSC} = 360MHz$), $R_{AMP} = 2540\Omega$ ($I_{OUT} = 50mA_{P-P} = 2540\Omega$) and $I_{OUT} = 50mA_{P-P} = 2540\Omega$ ($I_{OUT} = 50mA_{P-P} = 2540\Omega$) and $I_{OUT} = 50mA_{P-P} = 2540\Omega$ ($I_{OUT} = 50mA_{P-P} = 2540\Omega$) and $I_{OUT} = 50mA_{P-P} = 2540\Omega$) and $I_{OUT} = 50mA_{P-P} = 2540\Omega$ ($I_{OUT} = 50mA_{P-P} = 2540\Omega$) and $I_{OUT} = 50mA_{P-P} = 2540\Omega$) and $I_{$ measured at 60MHz), $V_{OUT} = 2.2V$

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
Fosc	Frequency Tolerance	Unit-unit frequency variation	310	358	400	MHz
F <sub>HIGH</sub>	Frequency Range High	$R_{FREQ} = 3.3k\Omega$		566		MHz
F <sub>LOW</sub>	Frequency Range Low	$R_{FREQ} = 18.2k\Omega$		100		MHz
TCOSC	Frequency Temperature Sensitivity	0°C to +70°C ambient		50		ppm/°C
PSRROSC	Frequency Change ΔF/F	V <sub>DD</sub> from 4.5V to 5.5V		1		%

### **Driver Characteristics**

 $V_{DD} = +5V, T_{A} = 25^{\circ}C, \ R_{L} = 10\Omega, \ R_{FREQ} = 30.5k\Omega \ (F_{OSC} = 60MHz), \ R_{AMP} = 2540\Omega \ (I_{OUT} = 50mA_{P-P} = 1000)$ measured at 60MHz), VOUT = 2.2V

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
AMP <sub>HIGH</sub>	Amplitude Range High	$R_{AMP} = 1.27k\Omega$		100		mA <sub>P-P</sub>
AMP <sub>LOW</sub>	Amplitude Range Low	$R_{AMP} = 12.7k\Omega$		10		mA <sub>P-P</sub>
IOS <sub>NOM</sub>	Offset Current @ 2.2V	$R_{FREQ} = 5210\Omega$ , $V_{OUT} = 2.2V$		-4		mA
IOS <sub>HIGH</sub>	Offset Current @ 2.8V	$R_{FREQ} = 5210\Omega$ , $V_{OUT} = 2.8V$		-4.8		mA
IOS <sub>LOW</sub>	Offset Current @ 1.8V	$R_{FREQ} = 5210\Omega$ , $V_{OUT} = 1.8V$		-3.5		mA
I <sub>OUTP-P</sub>	Output Current Tolerance	Defined as one standard deviation		2		%
Duty Cycle	Output Push Time/Cycle Time	$R_{FREQ} = 5210\Omega$		43		%
PSRR <sub>AMP</sub>	Amplitude Change of Output ΔI/I	V <sub>DD</sub> from 4.5V to 5.5V		-54		dB

# EL6208

### **Driver Characteristics**

 $V_{DD}=+5V,\,T_{A}=25^{\circ}C,\,R_{L}=10\Omega,\,R_{FREQ}=30.5k\Omega\;(F_{OSC}=60MHz),\,R_{AMP}=2540\Omega\;(I_{OUT}=50mA_{P-P})$  measured at 60MHz),  $V_{OUT}=2.2V$  (Continued)

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
T <sub>ON</sub>	Auto Turn-on Time	Output voltage step from 0V to 2.2V		15		μs
T <sub>OFF</sub>	Auto Turn-off Time	Output voltage step from 2.2V to 0V		0.5		μs
IOUT <sub>N</sub>	Output Current Noise Density	R <sub>FREQ</sub> = 5210Ω, measured @ 10MHz		2.5		nA/√Hz

# Pin Descriptions

PIN NAME	PIN TYPE	PIN DESCRIPTION
1	VDD	Positive power for laser driver (4.5V - 5.5V)
2	RFREQ	Set pin for oscillator frequency
3	RAMP	Set pin for output current amplitude
4	IOUT1	Current output to laser diode
5	GND1	Chip ground pin (0V for output)
6	IOUT2	Current output to laser diode

# I<sub>OUT</sub> Control

V <sub>OUT</sub>	I <sub>ОИТ</sub>
Less than V <sub>CUTOFF</sub>	OFF
More than V <sub>CUTOFF</sub>	Normal Operation

# **Typical Performance Curves**

 $V_{DD} = 5 \text{V}, \text{ T}_{A} = 25 ^{\circ}\text{C}, \text{ R}_{L} = 10 \Omega, \text{ R}_{FREQ} = 5.21 \text{k}\Omega, \text{ R}_{AMP} = 2.54 \text{k}\Omega, \text{ V}_{OUT} = 2.2 \text{V} \text{ unless otherwise specified}.$ 

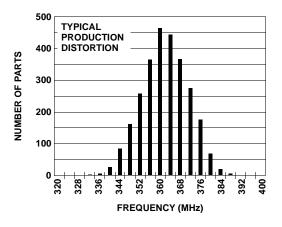


FIGURE 1. FREQUENCY DISTRIBUTION

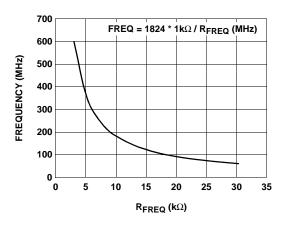


FIGURE 3. FREQUENCY vs R<sub>FREQ</sub>

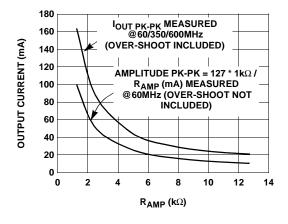


FIGURE 5. OUTPUT CURRENT vs RAMP

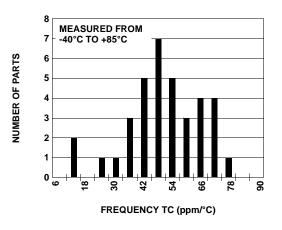


FIGURE 2. FREQUENY DRIFT with TEMPERATURE

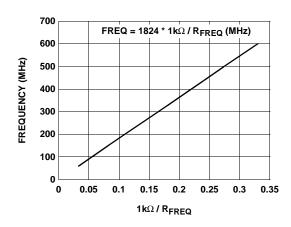


FIGURE 4. FREQUENCY vs 1 / RFREQ

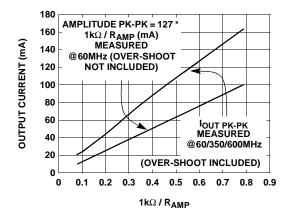


FIGURE 6. OUTPUT CURRENT vs 1 / RAMP

# Typical Performance Curves (Continued)

 $V_{DD}$  = 5V,  $T_A$  = 25°C,  $R_L$  = 10 $\Omega$ ,  $R_{FREQ}$  = 5.21k $\Omega$ ,  $R_{AMP}$  = 2.54k $\Omega$ ,  $V_{OUT}$  = 2.2V unless otherwise specified.

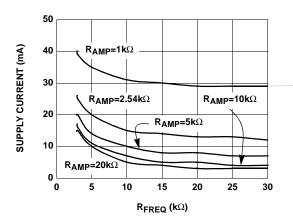


FIGURE 7. SUPPLY CURRENT vs RFREQ

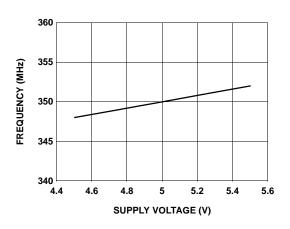


FIGURE 9. FREQUENCY vs SUPPLY VOLTAGE

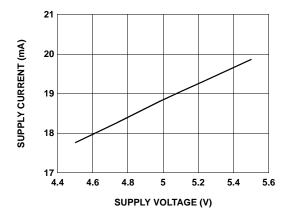


FIGURE 11. SUPPLY CURRENT vs SUPPLY VOLTAGE

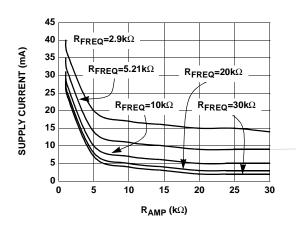


FIGURE 8. SUPPLY CURRENT vs R<sub>AMP</sub>

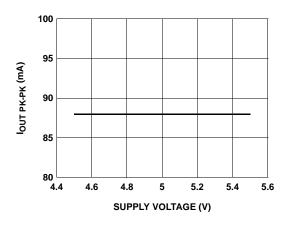


FIGURE 10. PEAK-TO-PEAK OUTPUT CURRENT vs SUPPLY VOLTAGE

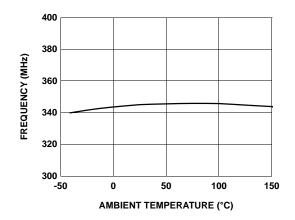


FIGURE 12. FREQUENCY vs TEMPERATURE

# Typical Performance Curves (Continued)

 $V_{DD} = 5 \text{V}, \text{ T}_{A} = 25 ^{\circ}\text{C}, \text{ R}_{L} = 10 \Omega, \text{ R}_{FREQ} = 5.21 \text{k}\Omega, \text{ R}_{AMP} = 2.54 \text{k}\Omega, \text{ V}_{OUT} = 2.2 \text{V} \text{ unless otherwise specified}.$ 

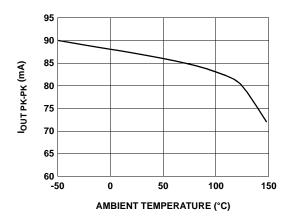


FIGURE 13. PEAK-TO-PEAK OUTPUT CURRENT vs TEMPERATURE

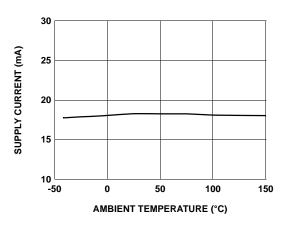


FIGURE 14. SUPPLY CURRENT vs TEMPERATURE

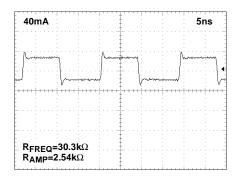


FIGURE 15. OUTPUT CURRENT @60MHz

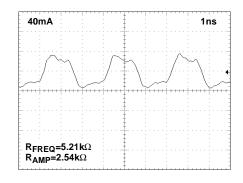


FIGURE 16. OUTPUT CURRENT @350MHz

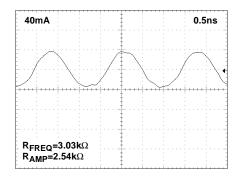


FIGURE 17. OUTPUT CURRENT @600MHz

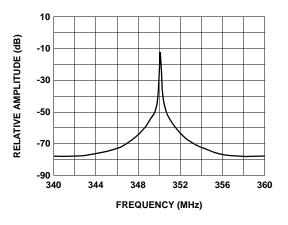
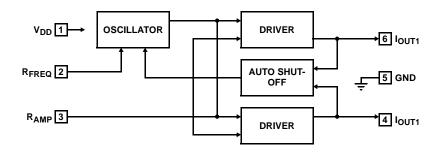
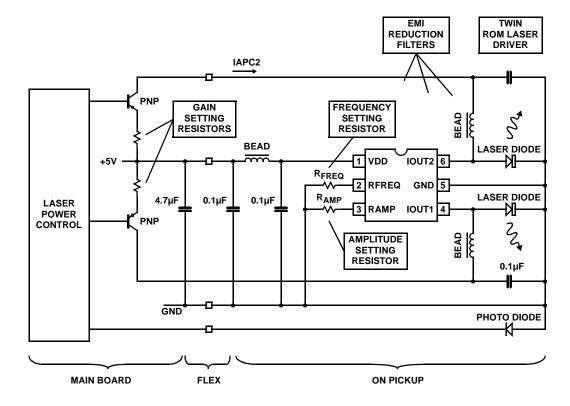


FIGURE 18. OUTPUT SPECTRUM - WIDEBAND

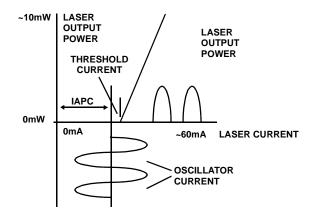
# **Block Diagram**



# Typical Application Diagram



# **Typical Waveforms**



### Applications Information

### **Product Description**

The EL6208 is a solid state, low-power, high-speed laser modulation oscillator with external resistor-adjustable operating frequency and output amplitude. It is designed to interface easily to laser diodes to break up optical feedback resonant modes and thereby reduce laser noise. The output of the EL6208 is composed of a push-pull current source, switched alternately at the oscillator frequency. The output and oscillator are automatically disabled for power saving when the average laser voltage drops to less than 1.1V. The EL6208 has the operating frequency from 60MHz to 600MHz and the output current from 10mAp\_p to 100mAp\_p. The supply current is only 18.5mA for the output current of 50mAp\_p at the operating frequency of 350MHz.

### Theory of Operation

A typical semiconductor laser will emit a small amount of incoherent light at low values of forward laser current. But after the threshold current is reached, the laser will emit coherent light. Further increases in the forward current will cause rapid increases in laser output power. A typical threshold current is 35mA and a typical slope efficiency is 0.7mW/mA.

When the laser is lasing, it will often change its mode of operation slightly, due to changes in current, temperature, or optical feedback into the laser. In a DVD-ROM, the optical feedback from the moving disk forms a significant noise factor due to feedback-induced mode hopping. In addition to the mode hopping noise, a diode laser will roughly have a constant noise level regardless of the power level when a threshold current is exceeded.

The oscillator is designed to produce a low noise oscillating current that is added to the external DC current. The effective AC current is to cause the laser power to change at the oscillator frequency. This change causes the laser to go through rapid mode hopping. The low frequency component of laser power noise due to mode hopping is translated up to sidebands around the oscillator frequency by this action. Since the oscillator frequency can be filtered out of the low frequency read and serve channels, the net result is that the laser noise seems to be reduced. The second source of laser noise reduction is caused by the increase in the laser power above the average laser power during the pushingcurrent time. The signal-to-noise ratio (SNR) of the output power is better at higher laser powers because of the almost constant noise power when a threshold current is exceeded. In addition, when the laser is off during the pulling-current time, the noise is also very low.

### RAMP and RFREQ Value Setting

The laser should always have a forward current during operation. This will prevent the laser voltage from collapsing,

and ensure that the high frequency components reach the junction without having to charge the junction capacitance.

Generally it is desirable to make the oscillator currents as large as possible to obtain the greatest reduction in laser noise. But it is not a trivial matter to determine this critical value. The amplitude depends on the wave shape of the oscillator current reaching the laser junction.

If the output current is sinusoidal, and the components in the output circuit are fixed and linear, then the shape of the current will be sinusoidal. But the amount of current reaching the laser junction is a function of the circuit parasitics. These parasitics can result in a resonant increase in output depending on the frequency due to the junction capacitance and layout. Also, the amount of junction current causing laser emission is variable with frequency due to the junction capacitance. In conclusion, the sizes of the  $R_{AMP}$  and  $R_{FREQ}$  resistors must be determined experimentally. A good starting point is to take a value of  $R_{AMP}$  for a peak-to-peak current amplitude less than the minimum laser threshold current and a value of  $R_{FREQ}$  for an output current close to a sinusoidal wave form (refer to the proceeding performance curves).

# RAMP and RFREQ Pin Interfacing

Figure 19 shows an equivalent circuit of pins associated with the  $R_{AMP}$  and  $R_{FREQ}$  resistors.  $V_{REF}$  is roughly 1.27V for both  $R_{AMP}$  and  $R_{FREQ}$ . The  $R_{AMP}$  and  $R_{FREQ}$  resistors should be connected to the non-load side of the power ground to avoid noise pick-up. These resistors should also return to the EL6208's ground very directly to prevent noise pickup. They also should have minimal capacitance to ground. Trimmer resistors can be used to adjust initial operating points.

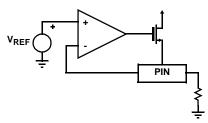


FIGURE 19. RAMP AND RFREQ PIN INTERFACE

External voltage sources can be coupled to the R<sub>AMP</sub> and R<sub>FREQ</sub> pins to effect frequency or amplitude modulation or adjustment. It is recommended that a coupling resistor of 1K be installed in series with the control voltage and mounted directly next to the pin. This will keep the inevitable high-frequency noise of the EL6208's local environment from propagating to the modulation source, and it will keep parasitic capacitance at the pin minimized.

#### Supply Bypassing and Grounding

The resistance of bypass-capacitors and the inductance of bonding wires prevent perfect bypass action, and 150mV<sub>P-P</sub>

noise on the power lines is common. There needs to be a lossy bead inductance and secondary bypass on the supply side to control signals from propagating down the wires. Figure 20 shows the typical connection.

L SERIES:  $70\Omega$  REACTANCE AT 300MHz

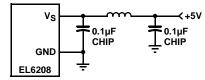


FIGURE 20. RECOMMENDED SUPPLY BYPASSING

Also important is circuit-board layout. At the EL6208's operating frequencies, even the ground plane is not low-impedance. High frequency current will create voltage drops in the ground plane. Figure 21 shows the output current loops.

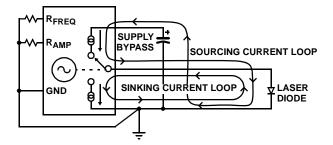


FIGURE 21. OUTPUT CURRENT LOOPS

For the pushing current loop, the current flows through the bypass capacitor, into the EL6208 supply pin, out the  $I_{OUT}$  pin to the laser, and from the laser back to the decoupling capacitor. This loop should be small.

For the pulling current loop, the current flows into the  $I_{OUT}$  pin, out of the ground pin, to the laser cathode, and from the laser diode back to the  $I_{OUT}$  pin. This loop should also be small.

### **Power Dissipation**

With the high output drive capability, the EL6208 is possible to exceed the 125°C "absolute-maximum junction temperature" under certain conditions. Therefore, it is important to calculate the maximum junction temperature for the application to determine if the conditions need to be modified for the oscillator to remain in the safe operating area.

The maximum power dissipation allowed in a package is determined according to:

$$\mathsf{P}_{\mathsf{DMAX}} = \frac{\mathsf{T}_{\mathsf{JMAX}} \cdot \mathsf{T}_{\mathsf{AMAX}}}{\Theta_{\mathsf{JA}}}$$

where:

P<sub>DMAX</sub> = Maximum power dissipation in the package

T<sub>JMAX</sub> = Maximum junction temperature

T<sub>AMAX</sub> = Maximum ambient temperature

 $\theta_{JA}$  = Thermal resistance of the package

The supply current of the EL6208 depends on the peak-to-peak output current and the operating frequency which are determined by resistors  $R_{AMP}$  and  $R_{FREQ}$ . The supply current can be predicted approximately by the following equation:

$$I_{SUP} \, = \, \frac{31.25 \, mA \times 1k\Omega}{R_{AMP}} + \frac{30 \, mA \times 1k\Omega}{R_{FREQ}} + 0.6 \, mA$$

The power dissipation can be calculated from the following equation:

$$P_D = V_{SUP} \times I_{SUP}$$

Here,  $V_{SUP}$  is the supply voltage. Figures 22 and 23 provide a convenient way to see if the device will overheat. The maximum safe power dissipation can be found graphically, based on the package type and the ambient temperature. By using the previous equation, it is a simple matter to see if PD exceeds the device's power derating curve. To ensure proper operation, it is important to observe the recommended derating curve shown in Figures 22 and 23. A flex circuit may have a higher  $\theta_{JA}$ , and lower power dissipation would then be required.

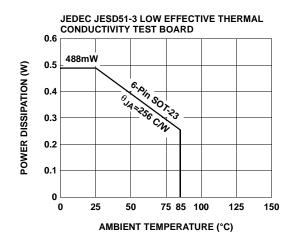


FIGURE 22. PACKAGE POWER DISSIPATION VS AMBIENT TEMPERATURE

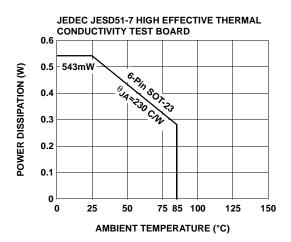


FIGURE 23. PACKAGE POWER DISSIPATION VS AMBIENT TEMPERATURE

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