

INA206 INA207 INA208

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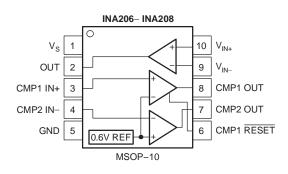
# High-Side Measurement Current-Shunt Monitor with Dual Comparators

# **FEATURES**

- COMPLETE CURRENT SENSE SOLUTION
- DUAL COMPARATORS:
  - Comparator 1 with Latch
  - Comparator 2 with Optional Delay
- COMMON-MODE RANGE: -16V to +80V
- HIGH ACCURACY: 3.5% (max) OVER TEMP
- BANDWIDTH: 500kHz
- QUIESCENT CURRENT: 1.8mA
- PACKAGES: SO-14, TSSOP-14, MSOP-10

# **APPLICATIONS**

- NOTEBOOK COMPUTERS
- CELL PHONES
- TELECOM EQUIPMENT
- AUTOMOTIVE
- POWER MANAGEMENT
- BATTERY CHARGERS
- WELDING EQUIPMENT



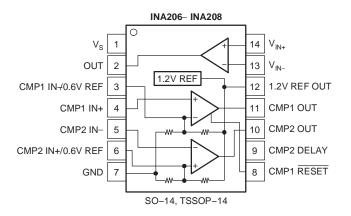
DEVICE	GAIN
INA206	20V/V
INA207	50V/V
INA208	100V/V

# DESCRIPTION

The INA206, INA207, and INA208 are a family of high-side, current-shunt monitors with voltage output, dual comparators, and voltage reference. The INA206, INA207, and INA208 can sense drops across shunts at common-mode voltages from –16V to +80V. The INA206, INA207, and INA208 are available with three output voltage scales: 20V/V, 50V/V, and 100V/V, with up to 500kHz bandwidth.

The INA206, INA207, and INA208 also incorporate two open-drain comparators with internal 0.6V references. On 14-pin versions, the comparator references can be overridden by external inputs. Comparator 1 includes a latching capability, and Comparator 2 has a user-programmable delay on 14-pin versions. 14-pin versions also provide a 1.2V reference output.

The INA206, INA207, and INA208 operate from a single +2.7V to +18V supply. They are specified over the extended operating temperature range of -40°C to +125°C.





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#### **ABSOLUTE MAXIMUM RATINGS(1)**

Supply Voltage, V+
Current-Shunt Monitor Analog Inputs, V <sub>IN+</sub> and V <sub>IN-</sub> :
Differential (V <sub>IN+</sub> ) – (V <sub>IN</sub> )
Common-Mode(2) –16V to +80V
Comparator Analog Input and Reset Pins(2):
GND – 0.3V to (V+) + 0.3V
Analog Output, Out $Pin^{(2)}$ GND – 0.3V to (V+) + 0.3V
Comparator Output, Out Pin <sup>(2)</sup> GND – 0.3V to 18V
V <sub>REF</sub> and CMP2 Delay PinGND – 0.3V to 10V
Input Current Into Any Pin <sup>(2)</sup> 5mA
Operating Temperature55°C to +150°C
Storage Temperature65°C to -150°C
Junction Temperature
ESD Ratings:
Human Body Model (HBM) 4000V
Charged Device Model (CDM)

- (1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not supported.
- (2) This voltage may exceed the ratings shown if the current at that pin is limited to 5mA.



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe

proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

#### ORDERING INFORMATION(1)

PRODUCT	GAIN	PACKAGE- LEAD	PACKAGE DESIGNATOR	PACKAGE MARKING	1.2V REF OUT	EXTERNAL COMP1 AND COMP2 REF INPUTS	INTERNAL COMP1 AND COMP2 0.6V REF	COMP2 DELAY PIN
INA206	20V/V	SO-14	D	INA206A	Х	Х	X	X
INA206	20V/V	TSSOP-14 <sup>(2)</sup>	PW	INA206A	Х	X	X	X
INAZUO	20 0 / 0	MSOP-10 <sup>(2)</sup>	DGS	BQQ			X	
INA207	50V/V	SO-14	D	INA207A	Х	X	X	X
INIA 207	INA207 50V/V	TSSOP-14 <sup>(2)</sup>	PW	INA207A	Х	Х	X	X
INAZU7		MSOP-10 <sup>(2)</sup>	DGS	BQR			X	
INA208	100V/V	SO-14	D	INA208A	Х	Х	X	Х
1114 000	400)////	TSSOP-14 <sup>(2)</sup>	PW	INA208A	Х	X	X	Х
INA208	100V/V	MSOP-10 <sup>(2)</sup>	DGS	BQS			Х	

<sup>(1)</sup> For the most current package and ordering information see the Package Option Addendum at the end of this document, or see the TI web site at www.ti.com.

<sup>(2)</sup> Available Q2 '07.



#### **ELECTRICAL CHARACTERISTICS**

**Boldface** limits apply over the specified temperature range,  $T_A = -40^{\circ}C$  to  $+125^{\circ}C$ .

At  $T_A$  = +25°C,  $V_S$  = +12V,  $V_{IN+}$  = 12V,  $V_{SENSE}$  = 100mV,  $R_L$  = 10k $\Omega$  to GND,  $R_{PULL-UP}$  = 5.1k $\Omega$  each connected from CMP1 OUT and CMP2 OUT to  $V_S$ , and CMP1 IN+ = 1V and CMP2 IN- = GND, unless otherwise noted.

CURRENT-SHUNT MONITOR			INA206, INA207, INA208			
PARAMETERS		CONDITIONS	MIN	TYP	MAX	UNIT
INPUT						
Full-Scale Sense Input Voltage	V <sub>SENSE</sub>	$V_{SENSE} = V_{IN+} - V_{IN-}$		0.15	(V <sub>S</sub> – 0.25)/Gain	٧
Common-Mode Input Range	V <sub>CM</sub>		-16		80	V
Common-Mode Rejection	CMR	$V_{IN+} = -16V \text{ to } +80V$	80	100		dB
over Temperature		$V_{IN+} = +12V \text{ to } +80V$	100	123		dB
Offset Voltage RTI <sup>(1)</sup>	Vos			±0.5	±2.5	mV
+25°C to +125°C					±3	mV
-40°C to +25°C					±3.5	mV
vs Temperature	dV <sub>OS</sub> /dT	T <sub>MIN</sub> to T <sub>MAX</sub>		5		μ <b>۷/</b> ° <b>C</b>
vs Power-Supply	PSR	$V_{OUT} = 2V, V_{IN+} = 18V, 2.7V$		2.5	100	μ <b>V/V</b>
Input Bias Current, V <sub>IN</sub> _ Pin	$I_{B}$			±9	±16	μ <b>Α</b>
OUTPUT (V <sub>SENSE</sub> ≥ 20mV)						
Gain: INA206	G			20		V/V
Gain: INA207				50		V/V
Gain: INA208				100		V/V
Gain Error		V <sub>SENSE</sub> = 20mV to 100mV		±0.2	±1	%
over Temperature		V <sub>SENSE</sub> = 20mV to 100mV			±2	%
Total Output Error <sup>(2)</sup>		$V_{SENSE} = 120$ mV, $V_{S} = +16$ V		±0.75	±2.2	%
over Temperature		$V_{SENSE} = 120$ mV, $V_{S} = +16$ V			±3.5	%
Nonlinearity Error <sup>(3)</sup>		$V_{SENSE} = 20$ mV to 100mV		±0.002		%
Output Impedance	$R_{O}$			1.5		Ω
Maximum Capacitive Load		No Sustained Oscillation		10		nF
OUTPUT (V <sub>SENSE</sub> < 20mV)(4)						
INA206, INA207, INA208		$-16V \le V_{CM} < 0V$		300		mV
INA206		$0V \le V_{CM} \le V_{S}, V_{S} = 5V$			0.4	V
INA207		$0V \le V_{CM} \le V_{S}, V_{S} = 5V$			1	V
INA208		$0V \le V_{CM} \le V_S$ , $V_S = 5V$			2	V
INA206, INA207, INA208		$V_S < V_{CM} \le 80V$		300		mV
VOLTAGE OUTPUT <sup>(5)</sup>						
Output Swing to the Positive I	Rail	$V_{IN-} = 11V, V_{IN+} = 12V$		(V+) - 0.15	(V+) - 0.25	V
Output Swing to GND <sup>(6)</sup>		$V_{IN-} = 0V, V_{IN+} = -0.5V$		$(V_{GND}) + 0.004$	$(V_{GND}) + 0.05$	٧
FREQUENCY RESPONSE						
Bandwidth: INA206	BW	$C_{LOAD} = 5pF$		500		kHz
Bandwidth: INA207		$C_{LOAD} = 5pF$		300		kHz
Bandwidth: INA208		$C_{LOAD} = 5pF$		200		kHz
Phase Margin		C <sub>LOAD</sub> < 10nF		40		Degrees
Slew Rate				1		V/μs
Settling Time (1%)		$V_{SENSE} = 10 \text{mV}_{PP} \text{ to } 100 \text{mV}_{PP},$ $C_{LOAD} = 5 \text{pF}$		2		μs
NOISE, RTI						
Output Voltage Noise Density				40		nV/√Hz

<sup>(1)</sup> Offset is extrapolated from measurements of the output at 20mV and 100mV V<sub>SENSE</sub>. (2) Total output error includes effects of gain error and V<sub>OS</sub>.

<sup>(3)</sup> Linearity is best fit to a straight line.

<sup>(4)</sup> For details on this region of operation, see the Accuracy Variations as a Result of V<sub>SENSE</sub> and Common-Mode Voltage section in the Applications Information.

<sup>(5)</sup> See Typical Characteristics curve Output Swing vs Output Current.

<sup>(6)</sup> Specified by design.



#### **ELECTRICAL CHARACTERISTICS**

**Boldface** limits apply over the specified temperature range,  $T_A = -40^{\circ}C$  to  $+125^{\circ}C$ .

At  $T_A = +25^{\circ}C$ ,  $V_S = +12V$ ,  $V_{IN+} = 12V$ ,  $V_{SENSE} = 100$ mV,  $R_L = 10$ k $\Omega$  to GND, and  $R_{PULL-UP} = 5.1$ k $\Omega$  each connected from CMP1 OUT and CMP2 OUT to  $V_S$ , unless otherwise noted.

		INA206, INA207, INA208			
COMPARATOR PARAMETERS	CONDITIONS	MIN	TYP	MAX	UNIT
OFFSET VOLTAGE					
Offset Voltage	Comparator Common-Mode Voltage = Threshold Voltage		2		mV
Offset Voltage Drift, Comparator 1			<u>±</u> 2		μ <b>۷/</b> °C
Offset Voltage Drift, Comparator 2			+5.4		μ <b>۷/</b> ° <b>C</b>
Threshold	T <sub>A</sub> = +25°C	590	600	610	mV
over Temperature		586		614	mV
Hysteresis(1), CMP1	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$		-8		mV
Hysteresis <sup>(1)</sup> , CMP2	$T_A = -40^{\circ}\text{C to } +85^{\circ}\text{C}$		8		mV
INPUT BIAS CURRENT(2)					
CMP1 IN+, CMP2 IN-			0.005	10	nA
vs Temperature				15	nA
INPUT IMPEDANCE					
Pins 3 and 6 (14-pin packages only)			10		kΩ
INPUT RANGE					
CMP1 IN+ and CMP2 IN-			0V to V <sub>S</sub> – 1.5V		V
Pins 3 and 6 (14-pin packages only) <sup>(3)</sup>			0V to V <sub>S</sub> – 1.5V		V
OUTPUT					
Large-Signal Differential Voltage Gain	CMP V <sub>OUT</sub> 1V to 4V, R <sub>L</sub> $\geq$ 15k $\Omega$ connected to 5V		200		V/mV
High-Level Output Current	$V_{ID} = 0.4V$ , $V_{OH} = V_{S}$		0.0001	1	μΑ
Low-Level Output Voltage	$V_{ID} = -0.6V$ , $I_{OL} = 2.35mA$		220	300	mV
RESPONSE TIME(4)					
Comparator 1	$R_L$ to 5V, $C_L$ = 15 pF, 100mV Input Step		1.3		μs
	with 5mV Overdrive		1.0		μο
Comparator 2	R <sub>L</sub> to 5V, C <sub>L</sub> = 15 pF, 100mV Input Step		1.3		μs
	with 5mV Overdrive, C <sub>DELAY</sub> Pin Open				·
RESET					
RESET Threshold(5)			1.1		V
Logic Input Impedance			2		ΜΩ
Minimum RESET Pulse Width			1.5		μs
RESET Propagation Delay			3		μs
Comparator 2 Delay Equation <sup>(6)</sup>	0 04.5		$C_{DELAY} = t_D/5$		μF
Comparator 2 Delay t <sub>D</sub>	$C_{DELAY} = 0.1 \mu F$		0.5		S

- (1) Hysteresis refers to the threshold (the threshold specification applies to a rising edge of a noninverting input) of a falling edge on the noninverting input of the comparator. Refer to Figure 1.
- (2) Specified by design.
- (3) See the Comparator Maximum Input Voltage Range section in the Applications Information.
- (4) The comparator response time specified is the interval between the input step function and the instant when the output crosses 1.4V.
- (5) RESET input has an internal 2MΩ (typical) pull-down. Leaving RESET open results in a LOW state, with transparent comparator operation.
- (6) The Comparator 2 delay applies to both rising and falling edges of the comparator output.

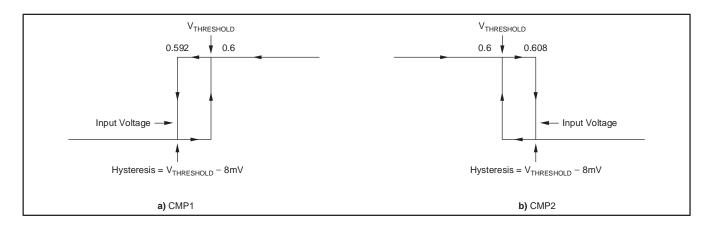


Figure 1. Comparator Hysteresis



#### **ELECTRICAL CHARACTERISTICS**

**Boldface** limits apply over the specified temperature range,  $T_A = -40^{\circ}C$  to  $+125^{\circ}C$ .

At  $T_A$  = +25°C,  $V_S$  = +12V,  $V_{IN+}$  = 12V,  $V_{SENSE}$  = 100mV,  $R_L$  = 10k $\Omega$  to GND, and  $R_{PULL-UP}$  = 5.1k $\Omega$  each connected from CMP1 OUT and CMP2 OUT to  $V_S$ , unless otherwise noted.

			INA	A206, INA207,	INA208	
REFERENCE PARAMETERS		CONDITIONS	MIN	TYP	MAX	UNIT
REFERENCE VOLTAGE						
1.2V <sub>REFOUT</sub> Output Voltag	je		1.188	1.2	1.212	V
Reference Drift	dV <sub>OUT</sub> /dT	$T_A = -40^{\circ}C$ to $+85^{\circ}C$		40	100	ppm/°C
0.6V <sub>REF</sub> Output Voltage (Pins 3 and 6 of 14-pin pac	kages only)			0.6		V
Reference Drift	dV <sub>OUT</sub> /dT	$T_A = -40^{\circ}C$ to $+85^{\circ}C$		40	100	ppm/°C
LOAD REGULATION	dV <sub>OUT</sub> /dl <sub>LOAD</sub>					
Sourcing		0mA < I <sub>SOURCE</sub> < 0.5mA		0.4	2	mV/mA
Sinking		$0mA < I_{SINK} < 0.5mA$		0.4		mV/mA
LOAD CURRENT	I <sub>LOAD</sub>			1		mA
LINE REGULATION	dV <sub>OUT</sub> /dV <sub>S</sub>	2.7V < V <sub>S</sub> < 18V		30		μV/V
CAPACITIVE LOAD						
Reference Output Max. Ca	pacitive Load	No Sustained Oscillations		10		nF
OUTPUT IMPEDANCE						
Pins 3 and 6 of 14-Pin Pack	kages Only			10		kΩ

#### **ELECTRICAL CHARACTERISTICS**

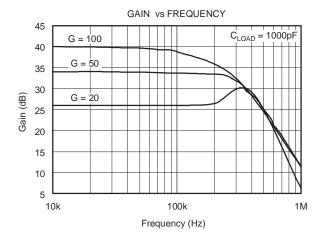
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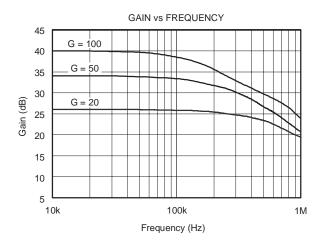
At  $T_A$  = +25°C,  $V_S$  = +12V,  $V_{IN+}$  = 12V,  $V_{SENSE}$  = 100mV,  $R_L$  = 10k $\Omega$  to GND,  $R_{PULL-UP}$  = 5.1k $\Omega$  each connected from CMP1 OUT and CMP2 OUT to  $V_S$ , and CMP1 IN+ = 1V and CMP2 IN- = GND, unless otherwise noted.

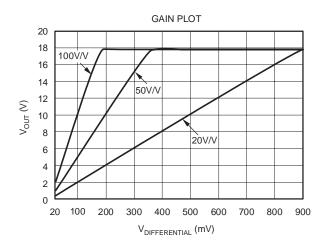
			INA206, INA207, INA208		INA208	
GENERAL PARAMETERS		CONDITIONS	MIN	TYP	MAX	UNIT
POWER SUPPLY						
Operating Power Supply	$v_s$		+2.7		+18	V
Quiescent Current	$I_Q$	V <sub>OUT</sub> = 2V		1.8	2.2	mA
over Temperature	-	$V_{OUT} = 2V$ $V_{SENSE} = 0mV$			2.8	mA
Comparator Power-On Reset Threshol	d(1)			1.5		V
TEMPERATURE						
Specified Temperature Range			-40		+125	°C
Operating Temperature Range			-55		+150	°C
Storage Temperature Range			-65		+150	°C
Thermal Resistance	$\theta_{\sf JA}$					
MSOP-10 Surface-Mount				200		°C/W
SO-14, TSSOP-14 Surface-Mount				150		°C/W

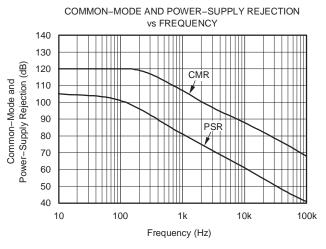
<sup>(1)</sup> The INA206, INA207, and INA208 are designed to power-up with the comparator in a defined reset state as long as CMP1 RESET is open or grounded. The comparator will be in reset as long as the power supply is below the voltage shown here. The comparator will assume a state based on the comparator input above this supply voltage. If CMP1 RESET is high at power-up, the comparator output comes up high and requires a reset to assume a low state, if appropriate.

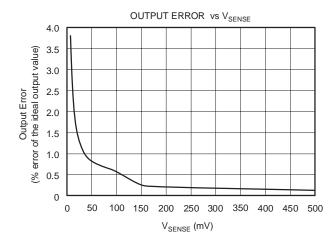
#### TYPICAL CHARACTERISTICS

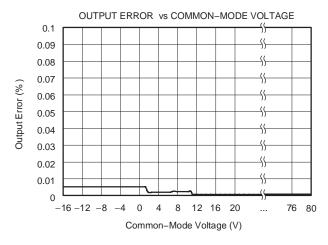




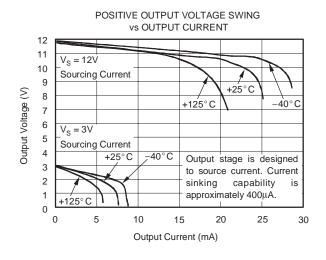


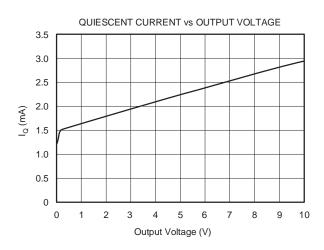


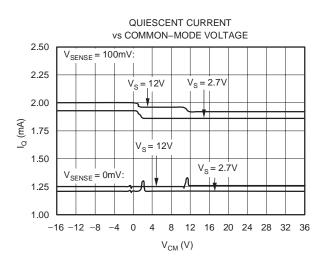


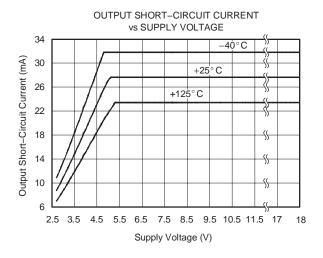


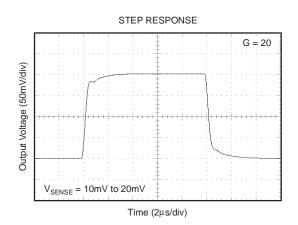


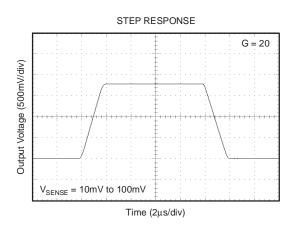






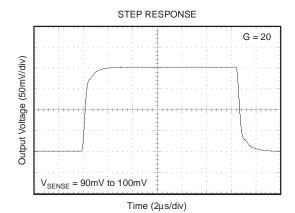


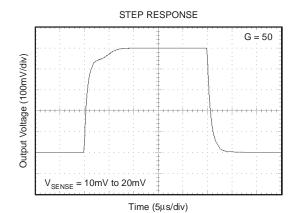




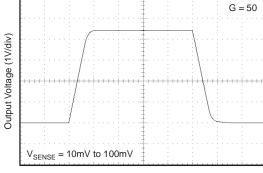


All specifications at T\_A = +25°C,  $V_S$  = +12V,  $V_{IN+}$  = 12V, and  $V_{SENSE}$  = 100mV, unless otherwise noted.

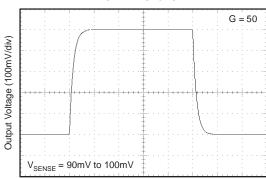




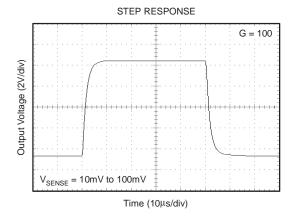




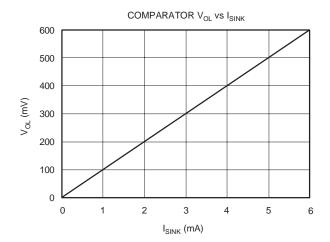




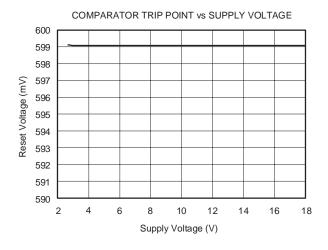
Time (5µs/div)

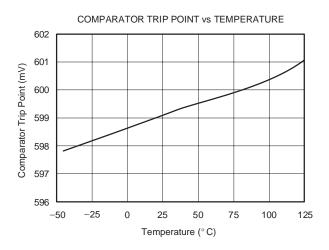


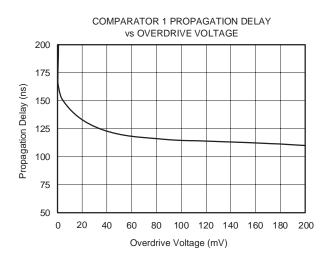
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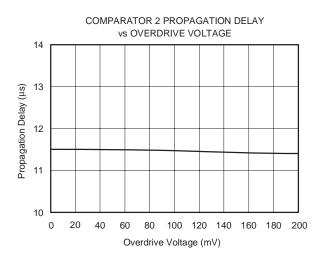


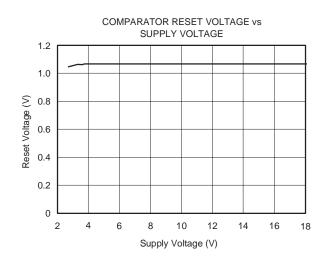


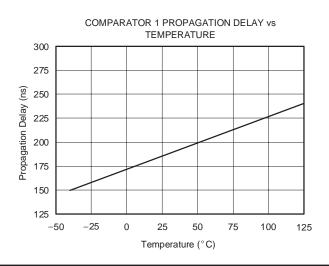




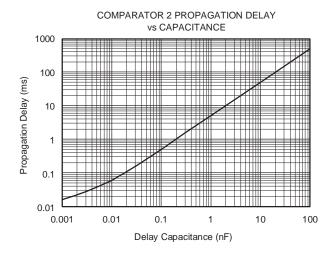


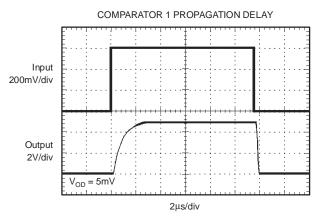


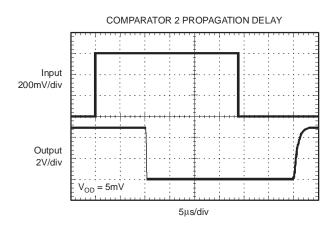


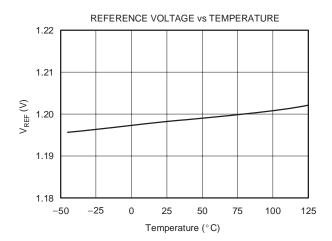














# APPLICATIONS INFORMATION

#### **BASIC CONNECTION**

Figure 2 shows the basic connection of the INA206, INA207, and INA208. The input pins,  $V_{\text{IN+}}$  and  $V_{\text{IN-}}$ , should be connected as closely as possible to the shunt resistor to minimize any resistance in series with the shunt resistance.

Power-supply bypass capacitors are required for stability. Applications with noisy or high impedance power supplies may require additional decoupling capacitors to reject power-supply noise. Connect bypass capacitors close to the device pins.

#### **POWER SUPPLY**

The input circuitry of the INA206, INA207, and INA208 can accurately measure beyond the power-supply voltage, V+. For example, the V+ power supply can be 5V, whereas the load power-supply voltage is up to +80V. The output voltage range of the OUT terminal, however, is limited by the voltages on the power-supply pin.

# ACCURACY VARIATIONS AS A RESULT OF VSENSE AND COMMON-MODE VOLTAGE

The accuracy of the INA206, INA207, and INA208 current shunt monitors is a function of two main variables:  $V_{SENSE}$  ( $V_{IN+} - V_{IN-}$ ) and common-mode voltage,  $V_{CM}$ , relative to the supply voltage,  $V_{S.}$   $V_{CM}$  is expressed as ( $V_{IN+} + V_{IN-}$ )/2; however, in practice,  $V_{CM}$  is seen as the voltage at  $V_{IN+}$  because the voltage drop across  $V_{SENSE}$  is usually small.

This section addresses the accuracy of these specific operating regions:

Normal Case 1:  $V_{SENSE} \ge 20$ mV,  $V_{CM} \ge V_{S}$ Normal Case 2:  $V_{SENSE} \ge 20$ mV,  $V_{CM} < V_{S}$ Low  $V_{SENSE}$  Case 1:  $V_{SENSE} < 20$ mV, -16V  $\le V_{CM} < 0$ Low  $V_{SENSE}$  Case 2:  $V_{SENSE} < 20$ mV, 0V  $\le V_{CM} \le V_{S}$ Low  $V_{SENSE}$  Case 3:  $V_{SENSE} < 20$ mV,  $V_{S} < V_{CM} \le 80$ V

#### Normal Case 1: $V_{SENSE} \ge 20 \text{mV}$ , $V_{CM} \ge V_{S}$

This region of operation provides the highest accuracy. Here, the input offset voltage is characterized and measured using a two-step method. First, the gain is determined by Equation (1).

$$G = \frac{V_{OUT1} - V_{OUT2}}{100mV - 20mV}$$
 (1)

where:

 $V_{OUT1}$  = Output Voltage with  $V_{SENSE}$  = 100mV  $V_{OUT2}$  = Output Voltage with  $V_{SENSE}$  = 20mV

Then the offset voltage is measured at  $V_{SENSE} = 100 \text{mV}$  and referred to the input (RTI) of the current shunt monitor, as shown in Equation (2).

$$V_{OS}RTI (Referred-To-Input) = \left(\frac{V_{OUT1}}{G}\right) - 100mV$$
 (2)

In the Typical Characteristics, the *Output Error vs Common-Mode Voltage* curve shows the highest accuracy for the this region of operation. In this plot,  $V_S = 12V$ ; for  $V_{CM} \ge 12V$ , the output error is at its minimum. This case is also used to create the  $V_{SENSE} \ge 20$ mV output specifications in the Electrical Characteristics table.

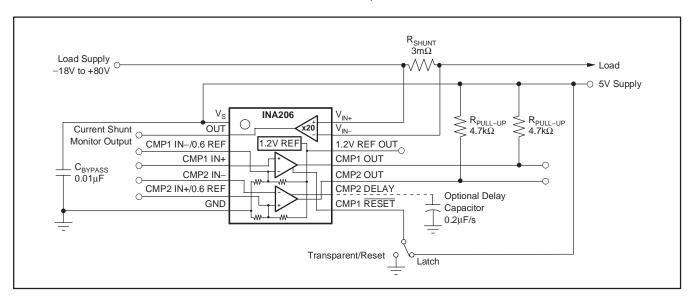


Figure 2. INA20x Basic Connection

#### Normal Case 2: $V_{SENSE} \ge 20 \text{mV}$ , $V_{CM} < V_{S}$

This region of operation has slightly less accuracy than Normal Case 1 as a result of the common-mode operating area in which the part functions, as seen in the *Output Error vs Common-Mode Voltage* curve. As noted, for this graph  $V_S = 12V$ ; for  $V_{CM} < 12V$ , the Output Error increases as  $V_{CM}$  becomes less than 12V, with a typical maximum error of 0.005% at the most negative  $V_{CM} = -16V$ .

Low  $V_{SENSE}$  Case 1:  $V_{SENSE} < 20 mV, -16 V \le V_{CM} < 0; \\ and Low \ V_{SENSE} Case 3: \\ V_{SENSE} < 20 mV, \ V_S < V_{CM} \le 80 V$ 

Although the INA206 family of devices are not designed for accurate operation in either of these regions, some applications are exposed to these conditions; for example, when monitoring power supplies that are switched on and off while  $V_{\rm S}$  is still applied to the INA206, INA207, or INA208. It is important to know what the behavior of the devices will be in these regions.

As  $V_{\text{SENSE}}$  approaches 0mV, in these  $V_{\text{CM}}$  regions, the device output accuracy degrades. A larger-than-normal offset can appear at the current shunt monitor output with a typical maximum value of  $V_{\text{OUT}} = 300 \text{mV}$  for  $V_{\text{SENSE}} = 0 \text{mV}$ . As  $V_{\text{SENSE}}$  approaches 20mV,  $V_{\text{OUT}}$  returns to the expected output value with accuracy as specified in the Electrical Characteristics. Figure 3 illustrates this effect using the INA208 (Gain = 100).

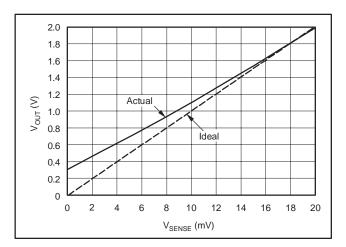


Figure 3. Example for Low  $V_{SENSE}$  Cases 1 and 3 (INA208, Gain = 100)

# Low $V_{SENSE}$ Case 2: $V_{SENSE}$ < 20mV, $0V \le V_{CM} \le V_{S}$

This region of operation is the least accurate for the INA206 family. To achieve the wide input common-mode voltage range, these devices use two op amp front ends in

parallel. One op amp front end operates in the positive input common-mode voltage range, and the other in the negative input region. For this case, neither of these two internal amplifiers dominates and overall loop gain is very low. Within this region, V<sub>OUT</sub> approaches voltages close to linear operation levels for Normal Case 2. This deviation from linear operation becomes greatest the closer V<sub>SENSE</sub> approaches 0V. Within this region, as V<sub>SENSE</sub> approaches 20mV, device operation is closer to that described by Normal Case 2. Figure 4 illustrates this behavior for the INA208. The V<sub>OUT</sub> maximum peak for this case is tested by maintaining a constant  $V_S$ , setting  $V_{SENSE} = 0$ mV and sweeping  $V_{CM}$  from 0V to  $V_{S}$ . The exact  $V_{CM}$  at which  $V_{OUT}$ peaks during this test varies from part to part, but the Vout maximum peak is tested to be less than the specified  $V_{OUT}$ Tested Limit.

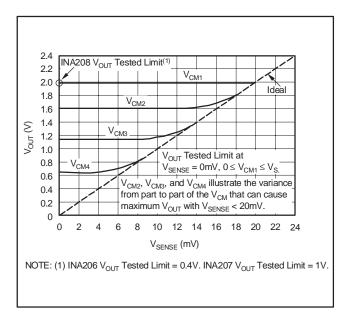


Figure 4. Example for Low V<sub>SENSE</sub> Case 2 (INA208, Gain = 100)

#### SELECTING RS

The value chosen for the shunt resistor,  $R_{\rm S}$ , depends on the application and is a compromise between small-signal accuracy and maximum permissible voltage loss in the measurement line. High values of  $R_{\rm S}$  provide better accuracy at lower currents by minimizing the effects of offset, while low values of  $R_{\rm S}$  minimize voltage loss in the supply line. For most applications, best performance is attained with an  $R_{\rm S}$  value that provides a full-scale shunt voltage range of 50mV to 100mV. Maximum input voltage for accurate measurements is 500mV.



#### TRANSIENT PROTECTION

The -16V to +80V common-mode range of the INA206. INA207, and INA208 is ideal for withstanding automotive fault conditions ranging from 12V battery reversal up to +80V transients, since no additional protective components are needed up to those levels. In the event that the INA206, INA207, and INA208 are exposed to transients on the inputs in excess of their ratings, then external transient absorption with semiconductor transient absorbers (zeners or Transzorbs) will be necessary. Use of MOVs or VDRs is not recommended except when they are used in addition to a semiconductor transient absorber. Select the transient absorber such that it will never allow the INA206, INA207, and INA208 to be exposed to transients greater than +80V (that is, allow for transient absorber tolerance, as well as additional voltage due to transient absorber dynamic impedance). Despite the use of internal zener-type ESD protection, the INA206, INA207, and INA208 do not lend themselves to using external resistors in series with the inputs since the internal gain resistors can vary up to ±30%. (If gain accuracy is not important, then resistors can be added in series with the INA206, INA207, and INA208 inputs with two equal resistors on each input.)

#### **OUTPUT VOLTAGE RANGE**

The output of the INA206, INA207, and INA208 is accurate within the output voltage swing range set by the power supply pin, V+. This performance is best illustrated when using the INA208 (a gain of 100 version), where a 100mV full-scale input from the shunt resistor requires an output voltage swing of +10V, and a power-supply voltage sufficient to achieve +10V on the output.

#### INPUT FILTERING

An obvious and straightforward location for filtering is at the output of the INA206, INA207, and INA208 series; however, this location negates the advantage of the low output impedance of the internal buffer. The only other option for filtering is at the input pins of the INA206, INA207, and INA208, which is complicated by the internal  $5 \mathrm{k} \Omega$  + 30% input impedance; this is shown in Figure 5. Using the lowest possible resistor values minimizes both the initial shift in gain and effects of tolerance. The effect on initial gain is given by Equation (3):

Gain Error% = 
$$100 - \left(100 \times \frac{5k\Omega}{5k\Omega + R_{FILT}}\right)$$
 (3)

Total effect on gain error can be calculated by replacing the  $5k\Omega$  term with  $5k\Omega-30\%$ , (or  $3.5k\Omega)$  or  $5k\Omega+30\%$  (or  $6.5k\Omega)$ . The tolerance extremes of  $R_{\text{FILT}}$  can also be inserted into the equation. If a pair of  $100\Omega$  1% resistors are used on the inputs, the initial gain error will be 1.96%. Worst-case tolerance conditions will always occur at the lower excursion of the internal  $5k\Omega$  resistor (3.5k $\Omega$ ), and the higher excursion of  $R_{\text{FILT}}-3\%$  in this case.

Note that the specified accuracy of the INA206, INA207, and INA208 must then be combined in addition to these tolerances. While this discussion treated accuracy worst-case conditions by combining the extremes of the resistor values, it is appropriate to use geometric mean or root sum square calculations to total the effects of accuracy variations.

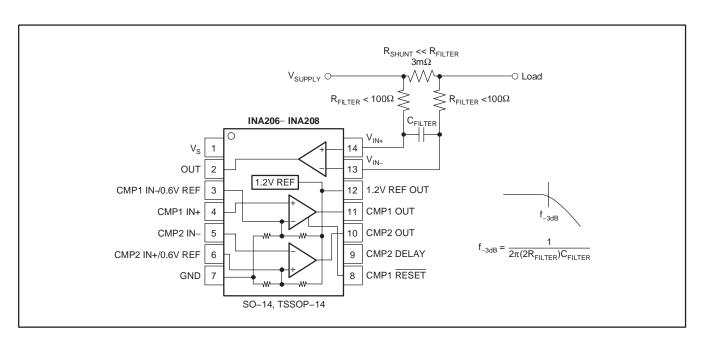


Figure 5. Input Filter (Gain Error – 1.5% to –2.2%)

#### REFERENCE

The INA206, INA207, and INA208 include an internal voltage reference that has a load regulation of 0.4mV/mA (typical), and not more than 100ppm/°C of drift. Only the 14-pin package allows external access to reference voltages, where voltages of 1.2V and 0.6V are both available. Output current versus output voltage is illustrated in the Typical Characteristics section.

#### **COMPARATOR**

The INA206, INA207, and INA208 devices incorporate two open-drain comparators. These comparators typically have 2mV of offset and a 1.3 $\mu$ s (typical) response time. The output of Comparator 1 latches and is reset through the CMP1 RESET pin, as shown in Figure 7. This configuration applies to both the 10- and 14-pin versions. Figure 6 illustrates the comparator delay.

The 14-pin versions of the INA206, INA207, and INA208 include additional features for comparator functions. The comparator reference voltage of both Comparator 1 and Comparator 2 can be overridden by external inputs for increased design flexibility. Comparator 2 has a programmable delay.

#### **COMPARATOR DELAY (14-Pin Version Only)**

The Comparator 2 programmable delay is controlled by a capacitor connected to the CMP2 Delay Pin; see Figure 2. The capacitor value (in  $\mu F$ ) is selected by using Equation (4):

$$C_{DELAY} (in \mu F) = \frac{t_D}{5}$$
 (4)

A simplified version of the delay circuit for Comparator 2 is shown in Figure 6. The delay comparator consists of two comparator stages with the delay between them. Note that I1 and I2 cannot be turned on simultaneously; I1 corresponds to a U1 low output and I2 corresponds to a U1

high output. Using an initial assumption that the U1 output is low, I1 is on, then U2 +IN is zero. If U1 goes high, I2 supplies 120nA to  $C_{DELAY}$ . The voltage at U2 +IN begins to ramp toward a 0.6V threshold. When the voltage crosses this threshold, the U2 output goes high while the voltage at U2 +IN continues to ramp up to a maximum of 1.2V when given sufficient time (twice the value of the delay specified for  $C_{DELAY}$ ). This entire sequence is reversed when the comparator outputs go low, so that returning to low exhibits the same delay.

It is important to note what will happen if events occur more rapidly that the delay timeout; for example, when the U1 output goes high (turning on I2), but returns low (turning I1 back on) prior to reaching the 0.6V transition for U2. The voltage at U2 +IN ramps back down at a rate determined by the value of  $C_{DELAY}$ , and only returns to zero if given sufficient time.

In essence, when analyzing Comparator 2 for behavior with events more rapid than its delay setting, use the model shown in Figure 6.

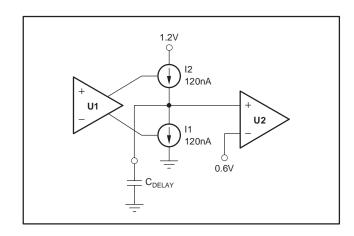


Figure 6. Simplified Model of the Comparator 2
Delay Circuit

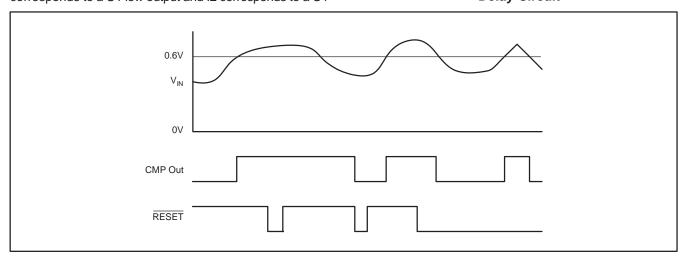


Figure 7. Comparator 1 Latching Capability



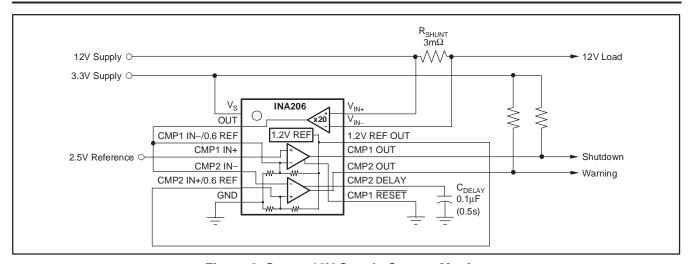


Figure 8. Server 12V Supply Current Monitor

# COMPARATOR MAXIMUM INPUT VOLTAGE RANGE

The maximum voltage at the comparator input for normal operation is up to (V+) - 1.5V. There are special considerations when overdriving the reference inputs (pins 3 and 6). Driving either or both inputs high enough to drive 1mA back into the reference introduces errors into the reference. Figure 9 shows the basic input structure. A general guideline is to limit the voltage on both inputs to a total of 20V. The exact limit depends on the available voltage and whether either or both inputs are subject to the large voltage. When making this determination, consider the  $20k\Omega$  from each input back to the comparator. Figure 10 shows the maximum input voltage that avoids creating a reference error when driving both inputs (an equivalent resistance back into the reference of  $10k\Omega$ ).

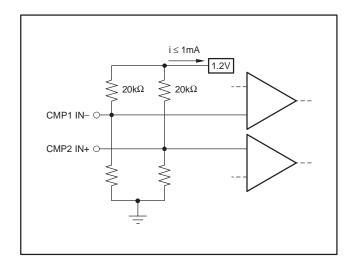


Figure 9. Limit Current Into Reference ≤ 1mA

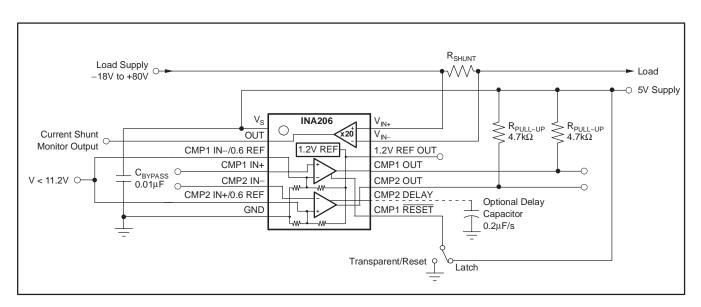


Figure 10. Overdriving Comparator Inputs Without Generating a Reference Error



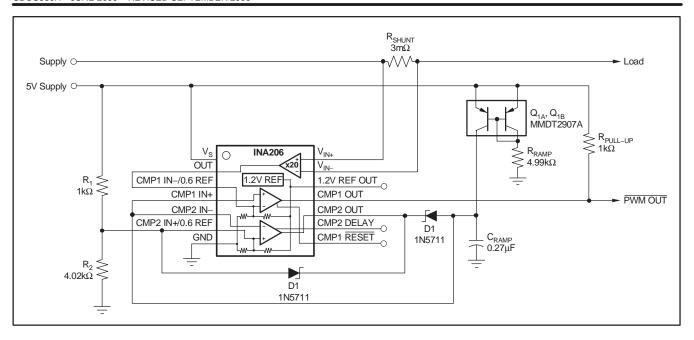


Figure 11. PWM Output Current-Shunt Monitor

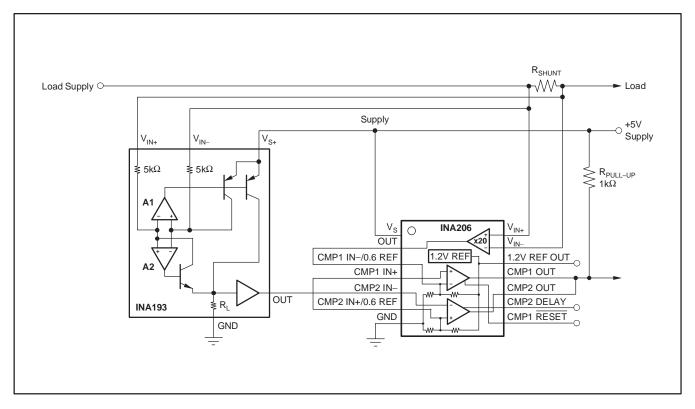


Figure 12. Bi-Directional Current Comparator



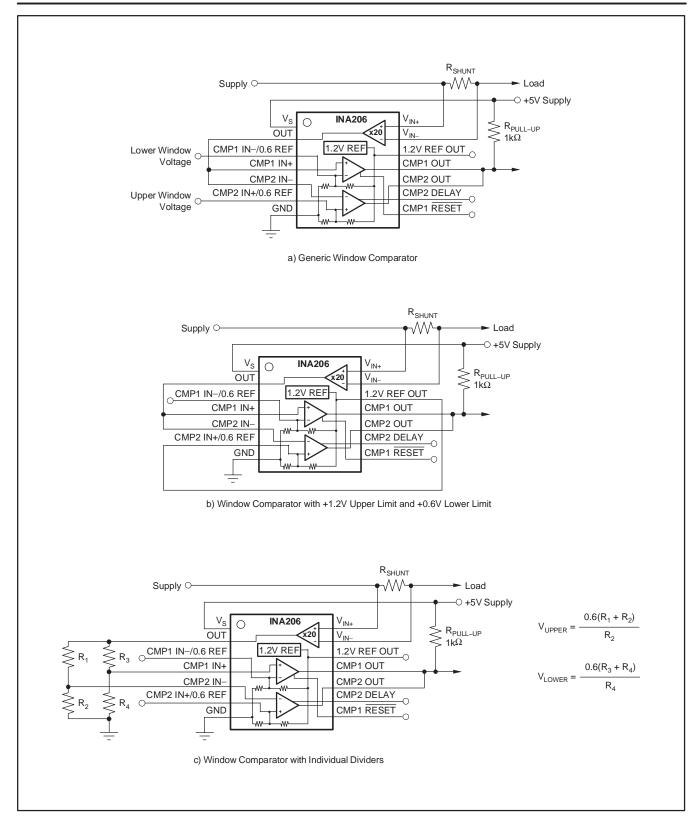


Figure 13. Using the INA206, INA207, and INA208 as Window Comparators



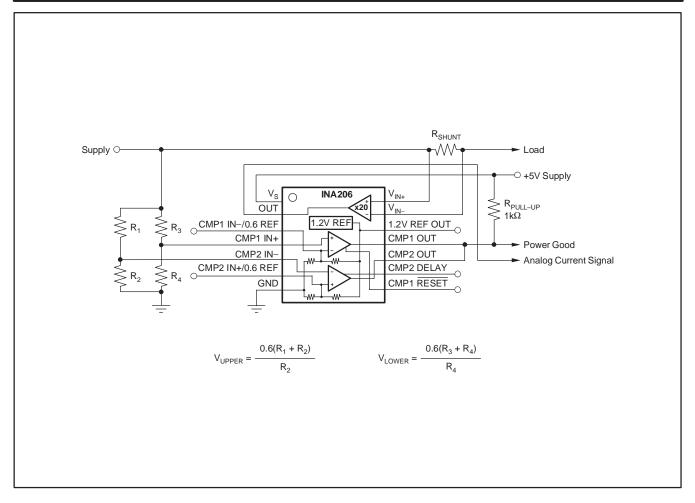


Figure 14. Analog Output Current-Shunt Monitor with Comparators Used as Power-Supply Under-Limit/Over-Limit or Power-Good Detector

# DGS (S-PDSO-G10)

# PLASTIC SMALL-OUTLINE PACKAGE



NOTES:

- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusion.
- D. Falls within JEDEC MO-187 variation BA.



# D (R-PDSO-G14)

# PLASTIC SMALL-OUTLINE PACKAGE



NOTES:

- A. All linear dimensions are in inches (millimeters).
- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusion not to exceed 0.006 (0,15).
- D. Falls within JEDEC MS-012 variation AB.



## PW (R-PDSO-G\*\*)

#### 14 PINS SHOWN

## PLASTIC SMALL-OUTLINE PACKAGE



NOTES: A. All linear dimensions are in millimeters.

B. This drawing is subject to change without notice.

C. Body dimensions do not include mold flash or protrusion not to exceed 0,15.

D. Falls within JEDEC MO-153

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